

The solution for your high modulus asphalt mixes

(High Modulus Asphalt HMA, High Modulus Asphalt Concrete HMAC, antirutting Semi Coarse Asphalt Concrete SCAC)

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Summary

- 1. Selenizza ® SLN specifications
- 2. Characterization of different natural bitumen
- 3. High modulus asphalt mixes
- 4. Implementation in road construction projects
- 5. Ways of introduction
- 6. Economic assessment
- 7. Environmental friendly
- 8. Production & reference sites
- 9. Conclusions



Selenizza ®SLN specifications

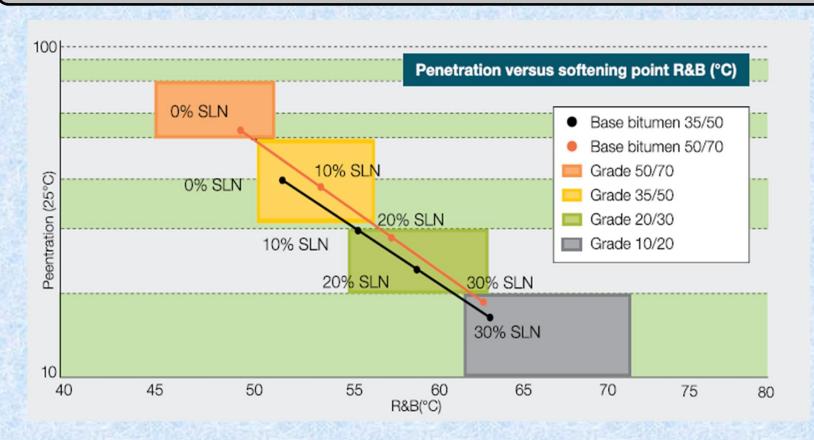
1

specifications

Penetration at 25°C (1/10 mm)	EN 1426	≤ 2
Softening point (R&B°C)	EN 1427	≤ 120
Penetration Index (IP)		> 3,0
Acidity Index (mg KOH/g)	NFT 66 013	3,5
Density at 25°C (g/cm³)	NFT 66 004	1,16
Asphaltene content (wt %)	- / 1	> 50
Mass loss at 163°C, 5 hours (%)	EN 13303	0,08



total binder modification



Depending on the added quantity of Selenizza and on the base bitumen, it is possible to **obtain precise penetration** and/or **R&B softening point** value of the resulting binder

total binder modification

<u>Principle</u>: The addition of Selenizza®SLN in a bituminous binder decreases the binder penetration and increases the binder softening point according to the added content, making their specifications move to the **harder** penetration grade specifications.

Typical examples:

50/70 base bitumen + (5 to 10 %) of Selenizza®SLN = 35/50 base bitumen

50/70 base bitumen + 15 % of Selenizza®SLN => (penetration **decreases 20-25** dmm +R&B **increases** 7-9 °C)

35/50 base bitumen + 15 % of Selenizza®SLN => (penetration **decreases 15-20** dmm +R&B **increases** 5-7 °C)

In **term of binder** in a mix design, **15%** of Selenizza®SLN by binder weight, represents some **0.9 to 1 %** with reference to the total weight of the asphalt mixture, with a binder content in the asphalt mix ranging from **5.8 to 6 %**.

Different sources of penetration grade bitumen could have slightly **different behaviours** against the addition of Selenizza SLN120[®] and so properties should **be checked** for different cases.



2

Skopje 2016 – Natural Asphalt Selenizza

- A study was carried out by the University of Rome "LA SAPIENZA" to characterize natural bitumen and evaluate their contribution to the modification of straight-run bitumen
- The aim of this research work was **to characterize** some of the natural asphalts, most diffused commercially and to evaluate their efficiency as modifiers
- Three natural asphalts were selected:

Natural asphalt	Bitumen content (%)	Asphaltènes content(%)	Penetration (à 25°C,1/10 mm)	R&B (°C)
Gilsonite	> 99	70	0	160-170
Selenizza	85-90	42*	0	115
Trinidad	53-55	33-37	1 - 4	93-98

An Iranian Straight Run bitumen (Gach Saran) with penetration 80-100, was added with each of the three types of natural asphalts:

by the percentage of 10% & at a minimum temperature of 150 – 180 °C



- In order to analyze the nature of the modification, two techniques have been used:
 - Dynamic rheological analysis
 - Modulated Differential Scanning Calorimetry (MDSC)
- The rheological analysis was carried out with a rotating rheometer under:
 - isochronal conditions, with temperature scanning, for the assessment of viscoelastic behavior in relatively high temperatures
 - isothermal conditions, with frequency scanning, for determining the characteristics in low temperature range
- The trails were performed in the respective linear viscoelastic areas for each sample in order to apply the temperature-frequency equivalency principle and generate the master curves.



Effect on Penetration and Softening Point

As expected, for the three cases, the resulting modified bitumen was characterized by **higher softening point** (R&B temperatures) and **lower penetration values**, compared to the original standard bitumen, due to the presence of high percentages of asphaltenes content in the natural asphalts.

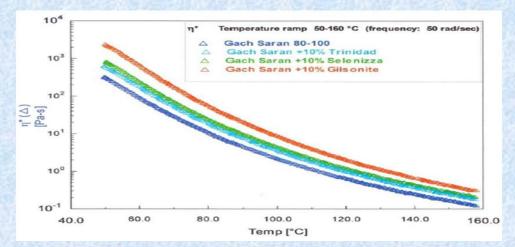
Type of bitumen	Penetration at 25* (1/10 mm)	R&BTemperature *C	Asphaltenes content (%)
Original bitumen	96	44	9,8
+10% Gilsonite	38	58	15,8
+10% Sel enizza	67	52	13,0
+10% Trin idad	78	51	12,3



Effect on viscoelastic properties at high temperatures

For medium and high temperatures (50 – 160°C), the rheological behavior whose softening point represent the lower limit, is not a function of the modifier quality and depends exclusively on the

asphaltenes content



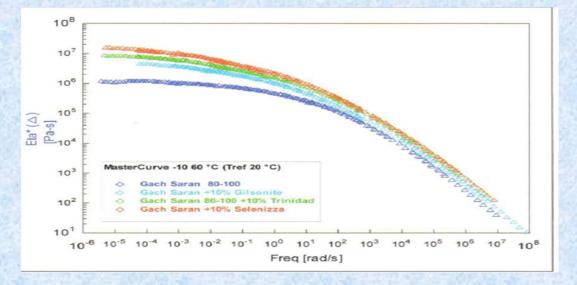
The viscosity values increase, the viscosity curves shift upwards, their shape and the slope remain unchanged and parallel for all sample types. The modifiers don't affect the internal interactions between the asphaltene components in the modified bitumen, which is a typical phenomenon for the compatible additives.



Effect on viscoelastic properties at low temperatures

For the **low temperatures (10 - 60°C)**, the rheological modifications seem complex and are

differentiated.



Master curves η^* , G',G'' = f(ω) drawn under reference temperatures 20°C & 60°C. The viscoelastic behavior and the ductility of the modified samples are impacted by the quality of the natural bitumen (bituminous+inorganic component). At **T=20°**, inversion of the zero shear viscosity η_0 (GS) < η_0 (Gil) < η_0 (Trid < η_0 (Sln)

Modulated Differential Scanning calorimetry MDSC:

➤ The samples (7 – 10 mg), were subjected to **a modulated** heating ramp resulting from a sinusoidal temperature ripple overlaid on a linear temperature ramp

$$dQ/dt = C_p \beta + f(T, t)$$

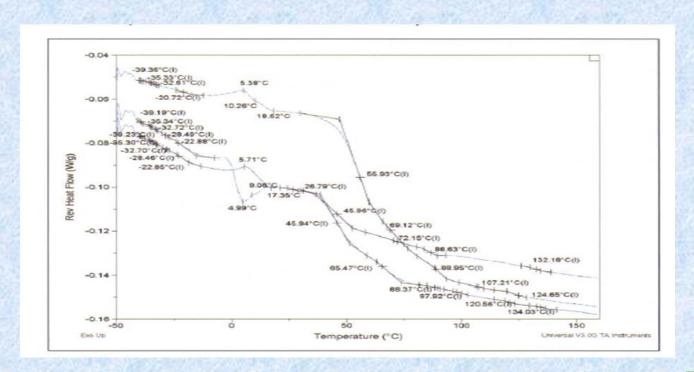
Temperature range: [-50 °C, + 160 °C]

- For the bitumen, the reversing curve $\approx 1/C_p$, is more indicative:
 - vitreous transitions
 - fusions



Modulated Differential Scanning calorimetry MDSC:

Reversing curves of the mixed samples





Modulated Differential Scanning calorimetry MDSC:

- ➤ The The MDSC analysis shows that the **rheological behavior** of the straight run bitumen is being **modified** by the addition of natural bitumen
- ➤ Trinidad & Selenizza: affect the lower limit of the softening range of the straight run bitumen (+55,8 °C → 45,9°C) due to the presence of different maltenic phases (of lower molar mass), which soften at lower temperatures. The asphaltenic phases, result to behave independently. A dilution effect of the original bitumen is obtained
- ➤ Gilsonite, does not act as a diluent, but expands the softening range to higher temperatures
- ➤ The modifications operate in such a way as to increase the **consistency**, **the viscosity** and the **stability** of the original bitumen → natural bitumen represent **an advantageous alternative** to other additives for modifying the road pavement bitumen



3

➤ Since the early 1980s, began to appear in the road construction sector, the **hot mix** asphalt structures with **high modulus** (> 12 000 MPa), which ensure **better resistance** to road **fatigue** and **permanent deformation** and facilitate the **reduction** of the road layer **thickness**

➤ With regard to **binder**, this mix design is usually obtained with **hard penetration grade** bitumen from **35/50** to **10/20** and/or the use of special additives to harden the bitumen or the mix



HMA > subbase

> bearing support

> mechanical resistance

> aggregates: 0/10, 0/14 ou 0/20 (most of the time granular 0/14)

binder: bitumen 10/20, 15/25 or 20/30 @ 5.5 - 6 %

Road Base Aspalt 1 & 2 **Hot Mix Asphalt Category 1 Hot Mix Asphalt Category 2** Duriez > 0.65 - 0.70 > 0.70 >0.75 Rutting < 10% (@ 10.000) < 7.5% (@ 30.000) < 7.5% (@ 30.000) Modulus > 9.000 MPa > 14.000 MPa > 14.000 MPa $> 80 - 90 \times 10^{-6}$ > 100 x 10⁻⁶ **Fatigue** > 130 × 10-6



Laying of a HMA with Selenizza SLN on a bank-run gravel for a logistic platform



HMAC > wearing course

- > skid resistance, drainage capacity
- > mechanical resistance and fatigue

> aggregates : 0/10 ou 0/14

binder : bitumen 20/30 @ 5.5 - 5.8 %

> Semi Coarse Asphalt Concrete 1, 2 & 3

Duriez > 0.75

Rutting < 10 - 7.5 - 5 % (@ 30.000)

Modulus > 5.500 - 7.000 MPa

Fatigue > 100 x 10^{-6}

Hot Mix Asphalt Concrete Category 1, 2 & 3

> 0.80

< 10 - 7.5 - 5 % (@ 30.000 cycles)

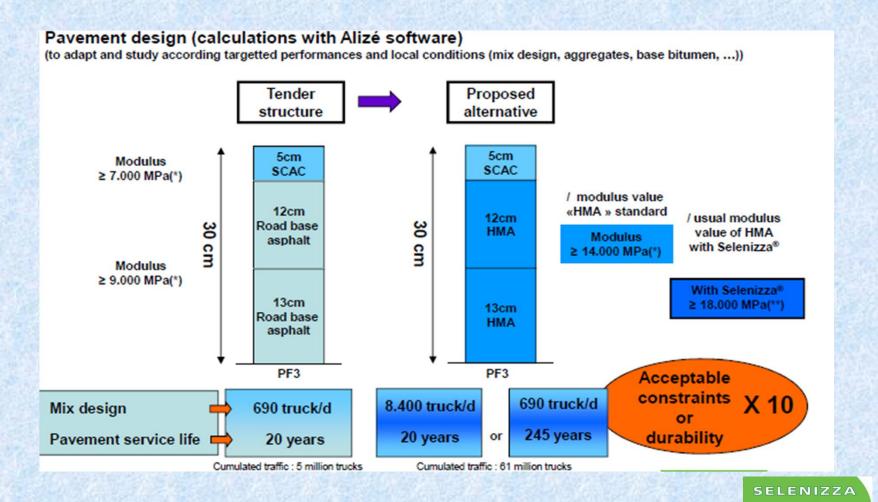
> 9.000 - 12.000 MPa

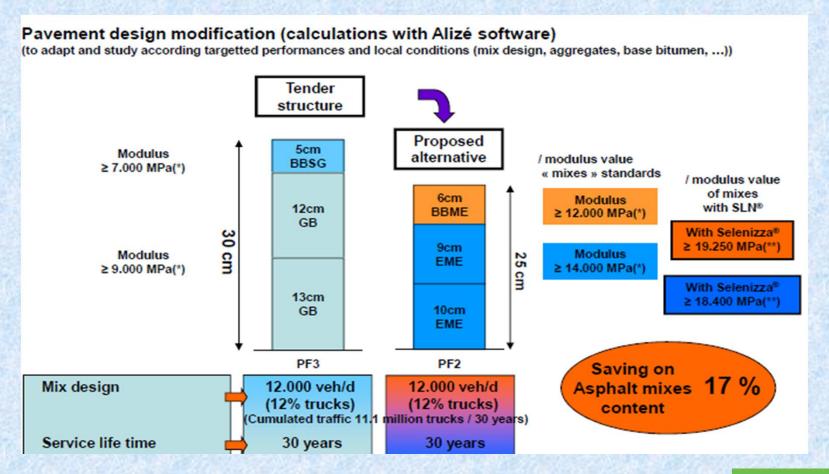
> 110 x 10-6



Laying of a HMAC with Selenizza®SLN on a road base asphalt for a city roundabout



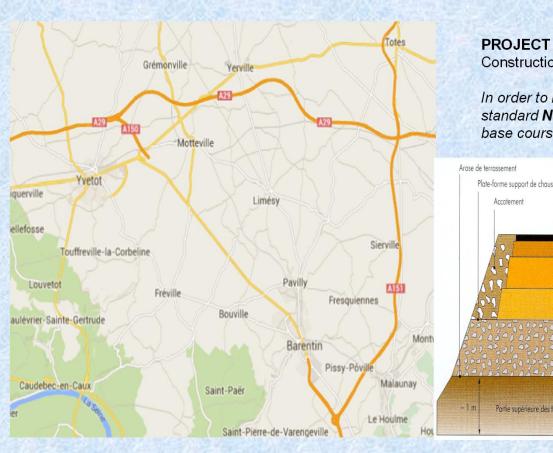






Implementation in road construction 4 projects

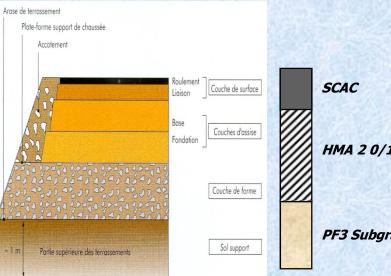
Skopje 2016 – Natural Asphalt Selenizza



PROJECT DESCRIPTION

Construction of a 17.5 km new roadway in A 150 Highway (FR)

In order to meet the technical specifications according to the CE standard NF EN 13108-1, the project proposes using a HMA base course EB 14 ASSISE 20/30 or HMA (EME) 0/14 class 2



6 cm

HMA 2 0/14 12 cm

PF3 Subgrade



For the manufacture of the recycled hot mix asphalt, two types of binders were analyzed:

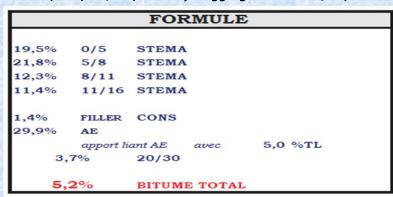
- The basic HMA mix design: 30% AE (asphalt aggregates) + 20/30 penetration grade bitumen
- Alternative studied: 30% AE (asphalt aggregates) + 50/70 grade bitumen + 1,5 % Selenizza
 Thresholds for HMA (EME) 0/14 class 2 validation

Type of asphalt mix	G.S.P. Voids content 100 gyrations %	r/R Water sensitivity	Resistance to rutting 60°C 30 000 cycles	Modulus 15°C 10 Hz MPa	Fatigue 10 ⁶ cycles μm/m
Test method	EN 12697-31	EN 12697-12	EN 12697-22	EN 12697-26	EN 12697-24
HMA class 2	≤ 6	≥ 0.75	≤ 7,5	≥ 14 000	≥ 130 x 10 ⁻⁶



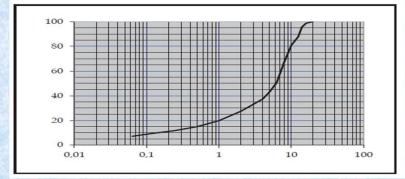
For comparision purposes, the HMA have been made with **the same composition** of materials in terms of **particle size distribution** curve and **% of binder** used

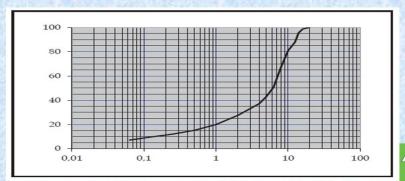
HMA(EME) 2 0/14 (30% recycl aggreg + bitume 20/30)



HMA(EME)2 0/14 (30% recycl aggreg + SLN + bitume 50/70)







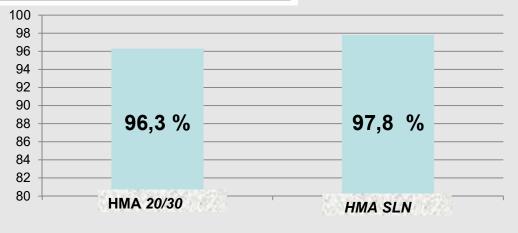
Water sensitivity

HMA 20/30

Sensibilité à l'Eau EN 12697-12 Méthode B			
COMPACITE	E 94,9% ESSAIS MECANIQUES		
INDICE VIDES	5,1%	C _D à 18° kPa	17918
MVRG t/m ³	2,767	C _W à 18° kPa	17250
MVR t/m ³ *	2,545	i/C (%)	96,3
MVA t/m ³	2,416	К	3,45

HMA SLN

Sensibilité à l'Eau EN 12697-12 Méthode B			
COMPACITE	95,1% ESSAIS MECANIQUES		
INDICE VIDES	4,9%	C _D à 18° kPa	20623
MVRG t/m ³	2,766	C _W à 18° kPa	20178
MVR t/m ³ *	2,544	i/C (%)	97,8
MVA t/m³	2,418	K	3,46



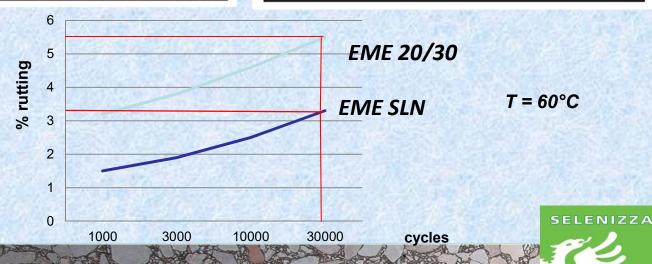
The 2 specimen were compacted at the same void percentage 5%



Resistance to rutting

ESSAI D'ORNIERAGE EN 12697-22			
% de vides des	éprouvettes 4,9	%	
N Cycles	% ornière moyen	Specific.	
1 000	3,2%		
3 000	3,8%		
10 000	4,6%		
30 000	5,5%	< 7,5%	

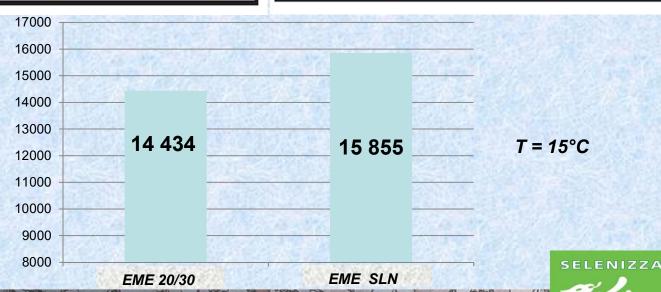
ESSAI D'ORNIERAGE EN 12697-22 % de vides des éprouvettes 4,7 %				
N Cycles	% ornière moyen	Specific.		
1 000	1,5%			
3 000	1,9%			
10 000	2,5%			
30 000	3,3%	< 7,5%		



Elastic modulus

TRACTION INDIRECTE	EN 12697-26 Annexe C
% de vides	5,1
Module 15°C, 124ms	14434
(MPa)	21101

TRACTION INDIRECTE EN 12697-26 Annexe C		
% de vides	5,0	
Module 15°C, 124ms	15855	
(MPa)	10000	



Fatigue

HMA 20/30

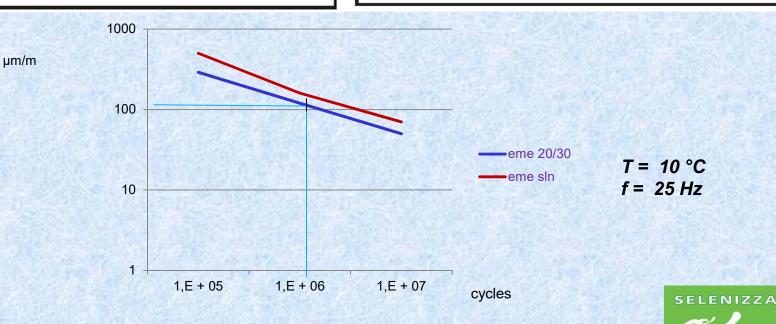
HMA SLN

ESSAI DE FATIGUE EN 12697-24 Annexe D

MVA (t/m3) : 5 % de vides Déformation relative à 10°,25Hz 134,1 μm/m

ESSAI DE FATIGUE EN 12697-24 Annexe D

MVA (t/m3): 5,1 % de vides Déformation relative à 10°,25Hz 137,3 μm/m



The study results **validaded the** approach which consisits in manufacturing the recycled HMA using a straigt run bitumen **50/70 + 1,5** % of natural bitumen *Selenizza*.





In order to respond to the technical challenge imposed by:

- High-level of traffic constraints
- Very harsh climatic conditions, with temperatures that oscillate between -20°C to + 40 °C

Switzerland incorporated in its national standard the concept of High Modulus Asphalt Mixes HMA.



The Swiss company COMIBIT from Canton Ticino, aiming to minimize the **rutting** and **cracking** phenomena in flexible pavement layers of the road network, characterized by an important traffic of trucks that cross the Alps, increasing from year to year, developed a new mix design of type AC EME 22C2 (class 2).

The new recipe improved **fatigue performance** using a polymer modified bitumen Shell Cariphalte 25 RC, while maintaining a **high modulus stiffness** using Selenizza as hardening additive.



In Switzerland, the performance class 1 of HMA, is recommended for improving the resistance to permanent deformations (rutting). The performance class 2, much harder to reach, has higher requirements of modulus of stiffness and resistance to fatigue

The Swiss standard specification SN 640 431-1NAB for AC EME 22

	Testing method	AC EME 22C1	AC EME 22C2
Voids content on Marshall specimens (%)	EN 12697-8	≤ 3.0 – 5.0	≤ 1.0 – 3.0
Water sensitivity	EN 12697-12	≥ 70	≥ 70
Binder content as a percentage of total mix weight (%)		≥ 4,6	≥ 5,4
Rutting resistance at 30 000 cycles & 60°C	EN 12697-22		
Rut depth on a slab of 10 cm thickness (%)		≤ 5.0	≤ 7.5
Complexe modulus at 15°C/10Hz (MPa)	EN 12697-26	≥ 11 000	≥ 14 000
Fatigue resistance at 10°C/25Hz (microdeformations)	EN 12697-24	≥ 100	≥ 135

Based on the **same grading curve**, two alternatives of mix design have been tested, containing different dosage levels of Selenizza, to determine its percentage for obtaining a final binder with penetration ranging between **10 to 20 dmm**.

- First formulation (Selenizza 26% of the total binder)
 3.9% Shell Cariphalte 25 RC+ 1.4% SLN = 5.3%
- 2. Second formulation (Selenizza 29% of the total binder)3.9% Shell Cariphalte 25 RC+ 1.6% SLN = 5.5%



Modulus and fatigue Test results

Bonder composition	Unity	Mix design 1	Mix design 2
Shell Cariphalte 25 RC	%	3,9	3,9
Selenizza SLN	%	1,4	1,6
Theoretical binder content ("% by mix mass)	%	5,3	5,5
Complex modulus at 15°C/10Hz (EN 12697-26)	MPa	19 441	18 336
Hydrostatic voids percentage (%)	%		
Fatigue resistance at 10°C/25Hz (EN 12697-24)	Microdef	139	145



The obtained modulus and fatigue tests results **clearly exceed** the Swiss standard specification for the asphalt mixes AC EME 22 C2 (14 000 MPa and 135 µdef).

To prevent the **cracking risk** at low temperatures, **a new job** mix formula was Implemented, where an **optimum value** of **stiffness modulus** was obtained by Introducing the correct percentage of Selenizza, maintaining a high level of fatigue resistance with a relatively less strong value of the stiffness modulus:

4.7% Shell Cariphalte 25 RC+ **1.4%** SLN = **6.1%**

The tests performed on **extracted binder** indicated that it belonged to a **10/20** paving grade bitumen: **penetration** = **13 dmm** and **TR&B** = **86,7°C**

High Performance Asphalt Mixtures in Switzerland

The results of tests performed by the LAVOC Laboratory at the Swiss Federal Institute of Technology Lausanne, confirmed that the new job mix formula met the technical requirements, with significantly higher values

 $\square \mathcal{E}_6$ (extrapoled) $\approx 150 \, \mu def$

☐ Modulus (15°C/10 Hz) = 15 100 MPa

(Swiss standard ≥135 µdef)

(Swiss standard ≥ 14 000 MPa)

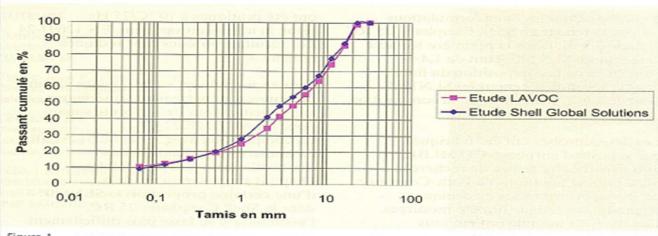


Figure 1 Courbes granulométriques des enrobés AC EME 22 testés

High Performance Asphalt Mixtures in Switzerland



Implementations in road construction projects: Highway Fier-Tepelene (AI)

The new road pavement structure, instead of **23 cm**, consisted of **19 cm** paving structure composed of three layers of continuously- graded bituminous mixtures:

base course
9 cm

binder course
6 cm

> wearing course 4 cm

For all bituminous mixtures, the natural bitumen Selenizza was used to a percentage of **8%** by weight of the base bitumen



Implementations in road construction projects: Highway Fier-Tepelene (AI)

- ➤ A study conducted by the Polytechnic University of Turin Italy, on materials sampled from the production plant, as well as on a test session, evaluated the binder and pavement performance.
- The analysis of compact issues, by referring to binder viscosity and the binder related contribution to the occurrence of rutting, fatigue and thermal cracking as well as the assessment of mixture stiffness, led to the conclusion that the considered bituminous mixtures containing the natural asphalt Selenizza, were in compliance with the pavement construction standards and specifications





Implementations in road construction projects: Highway A8 "Olimpia Odos" (Gr)

- The project involved the implementation of 375 km highway and was designed according to the prescription of **French Standards** applied to **Greek reality and experience**.
- The road structure consisted of :
 - DBM (Dense Bitumen Macadam) base course
 - anti-rutting binder course AC (5 cm)
 - anti-skid TAC (thin asphalt concrete) wearing course (2.5 cm).



Implementations in road construction projects: Highway A8 "Olimpia Odos" (Gr)

- > Several trial mix designs for the base and binder courses were tested using different kind of binders such as:
- bitumen 50/70
- bitumen 50/70 + 8% Selenizza
- bitumen 30/50
- PR PLAST modified bitumen.

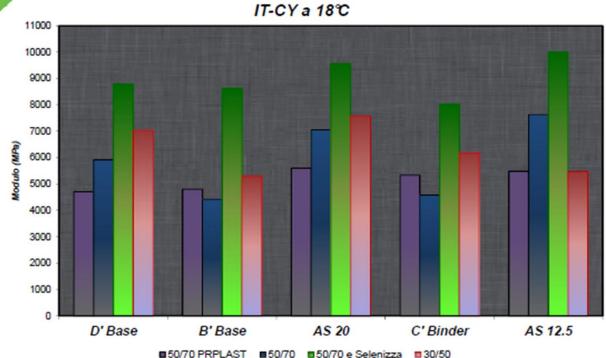


Highway A8 "Olimpia Odos" (Gr) STIFFNESS MODULUS (Indirect Tensile Test)



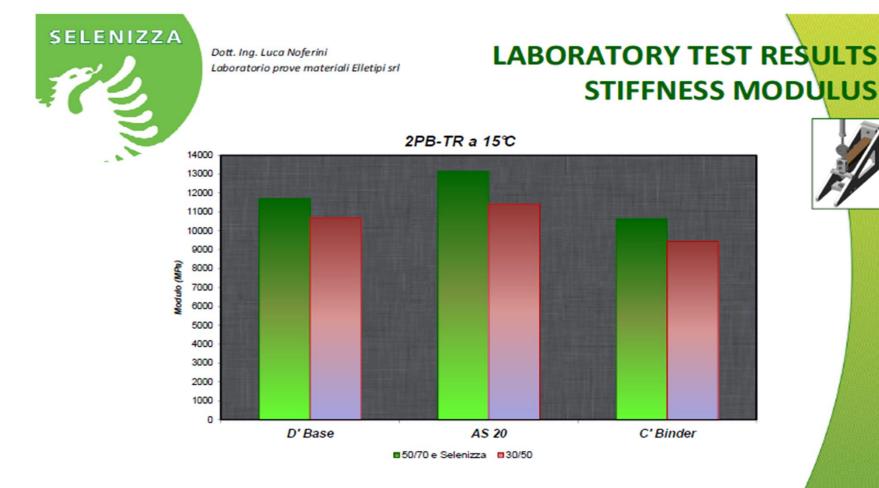
Dott. Ing. Luca Noferini Laboratorio prove materiali Elletipi srl

LABORATORY TEST RESULTS STIFFNESS MODULUS





Highway A8 "Olimpia Odos" (Gr) STIFFNESS MODULUS (Two Point Bending test)



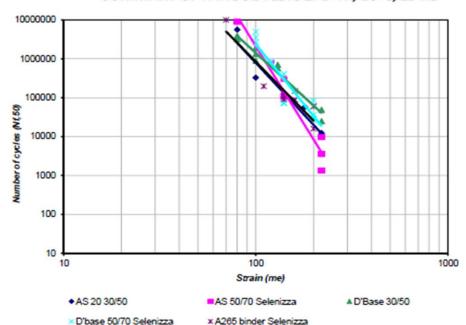
Highway A8 "Olimpia Odos" (Gr) FATIGUE TEST



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LABORATORY TEST RESULST FATIGUE RESISTANCE 2PB-TR

SUMMARY OF FATIGUE TESTS 2PB-TR, 10°C, 25 Hz



Material	Bituminous binder	Fatigue £6 10 °C, 25 Hz	Class asphalt mix
STS A265 B' binder course	50/70 + 8% Selenice Pen = 39	101.6	DBM4
STS A 260 D' base course	30/50 Pene = 45	108	DBM3
STS A 260 D' base course	50/70 + 8% Selenizza Pen=39	112	DBM4
AS 20 base course	50/70 + 8% Selenizza Pen = 39	110	DBM4
AS 20 base course	30/50 Pen= 45	95	DBM3

	TAC	AC	DBM2	DBM3	DBM4	HDM
10°C	7200	7200	12 300	12 300	14 550	17 000
18°C	4320	4320	7500	7500	8870	12200
ε6	-	-	80	90	100	130
-1/b	-	-	5	5	5	5
SN	-	-	0,3	0,3	0,3	0,25
v	0,35	0,35	0,35	0,35	0,35	0,35
Kc	-	-	1,3	1,3	1,3	111

Implementations in road construction projects: Highway A8 "Olimpia Odos" (Gr)

Laboratory tests on elastic modulus and fatigue showed that the binder with bitumen 50/70 + 8% Selenizza, had higher results of stiffness and fatigue compared to all the other tested binders, allowing to produce an asphalt concrete that belongs to the higher project category DBM 4, thereby making it possible to reduce the road package thickness by at least 4 cm.





Ways of introduction

5

Ways of introducing SELENIZZA in the asphalt plant

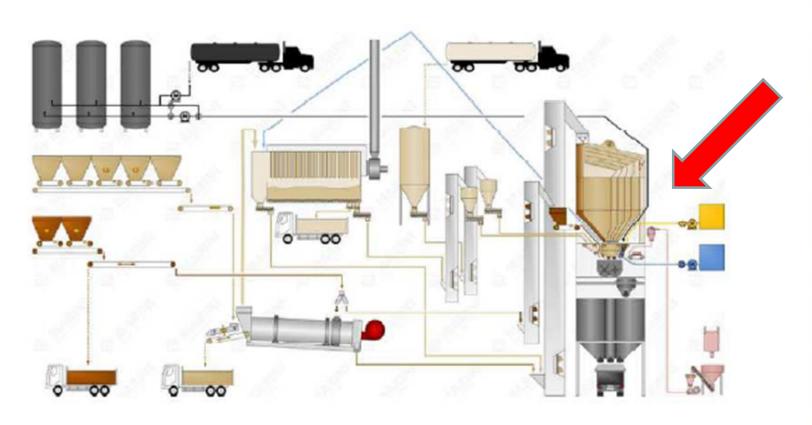
➤ Added in the *mixer* during the asphalt mixing process, in the **dicontinous** asphalt plants

Inserted into the recycling ring during the asphalt mixing process, in the continous asphalt plants

Blended directly with the hot bitumen in asphalt binder storage tanks



1. Introduced directly in the mixer of discontinuous asphalt mix plants





introducing SELENIZZA in the asphalt plant

pneumatic transport







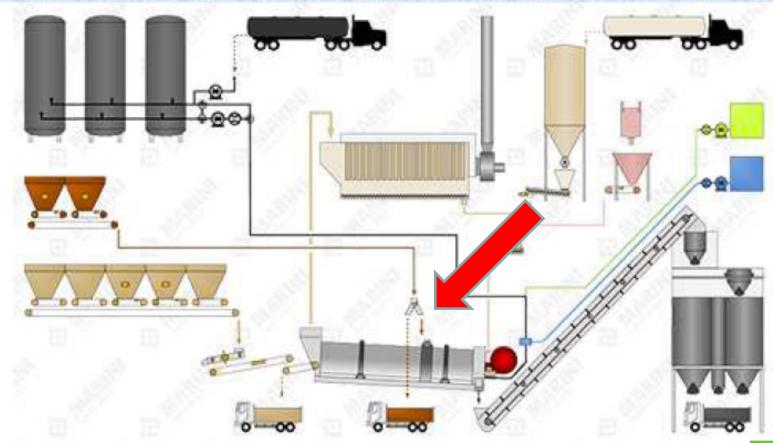
introducing SELENIZZA in the asphalt plant

mechanical insertion into the hopper via a belt conveyor or screw conveyor





2. Introduced via the recycling ring in the continuous asphalt plants





Introducing SELENIZZA in the asphalt plant



introducing SELENIZZA in the asphalt plant



insertion to the *recycling ring* during the asphalt mixing process, in the **continous** asphalt plants (300 tons /hours France) **Recyling + Selenizza**



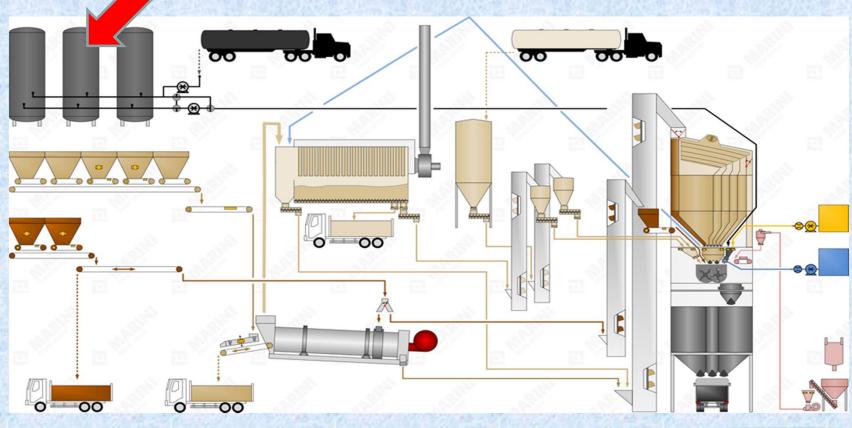
introducing in the asphalt plant Recyling + Selenizza



continous asphalt plant 300 tons /hours France

ELENIZZA

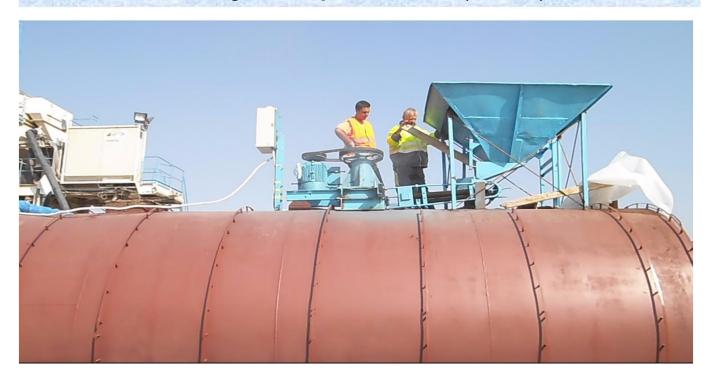
3. Added to the liquid asphalt binder in the stirred storage tank





introducing in the asphalt plant Recyling + Selenizza

Mixing with liquid bitumen (Serbia)





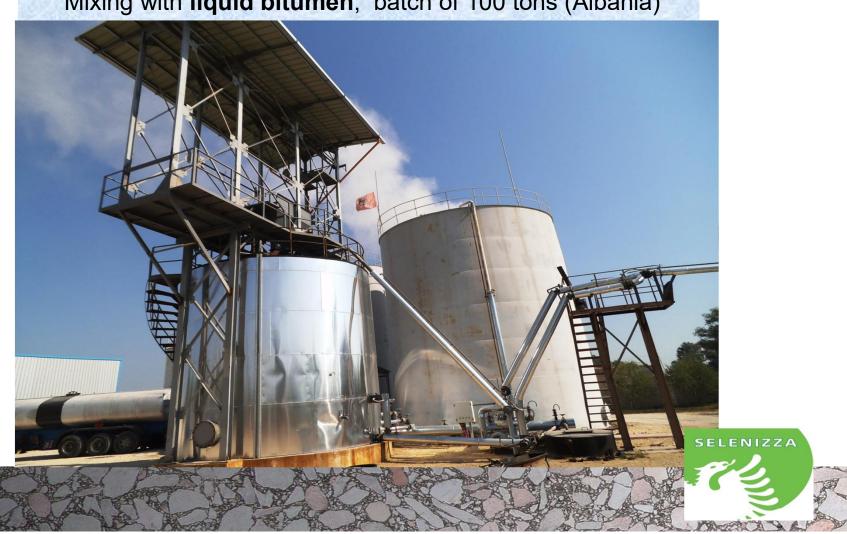
introducing in the asphalt plant Recyling + Selenizza

Blended directly with the hot bitumen in tanks (Serbia)



introducing in the asphalt plant Recyling + Selenizza

Mixing with liquid bitumen, batch of 100 tons (Albania)



introducing in the asphalt plant Recyling + Selenizza

Mixing with liquid bitumen directy in the tank of polymers (Greece)



Economic assessment

6

ECONOMIC ASSESSMENT Optimum binder content

Recently, a cost analysis was conducted by the Highway Institute of Belgrade (Serbia). For experimental purposes, were investigated and compared the characteristics and the manufacturing costs of a **carrying layer BNS 22s** (A) based on a conventional road bitumen BIT 60 (50/70) and the same mix design whose binder was composed of BIT 60 (50/70) + 10% natural bitumen Selenizza (relative to the total binder weight) Using the **Marshall method**, was deducted the **optimum binder content** for each mix design:

- > 3,5% for the asphalt mix with conventional binder
- > 3,3 % for the asphalt mix whose binder was modified with Selenizza



ECONOMIC ASSESSMENT Marshall Test

The addition of **Selenizza increases** the **Marshall quotient** (ratio of stability to flow):

	Stability [kN]	Flow [mm]	S/F [kN/mm]
Standard asphalt mixture	12.8	3.2	4
Asphalt mixture + Selenizza	14.1	2.8	5
Serbian standard	> 8.0	-	> 2.5

$$T = 60^{\circ}C$$
 voids= 5.9 %



ECONOMIC ASSESSMENT Stiffness Modulus

Test results show that the addition of Selenizza increases the stiffness modulus by at least 30% compared to the standard asphalt mixture

	Module E* [MPa]	Norme [MPa]
Standard asphalt mixture	6 585	≥ 3 600
Asphalt mixture + Selenizza	8 472	≥ 3 600



ECONOMIC ASSESSMENTPrices constituent materials & production

- Economic analysis was carried out based on the analysis of the prices of constituent materials and the prices of asphalt mixtures production with and without the addition of natural asphalt SELENIZZA.
- Prices of the constituent materials and production costs of asphalt mix were taken from asphalt plant AD "ROADS" Uzice in October 2014, without VAT.
- > The flexible pavement structure under analysis was composed of the following layers :

Surface Asphalt Concrete layer (AB 11s)

thickness = 5 cm

 Bituminous bearing course layer (BNS 22s A) (with and without addition of SELENIZZA) thickness = 8 cm

Unbound gravel layer 0/31.5 mm

thickness = 15cm

Unbound gravel layer 0/63 mm

thickness = 35cm



ECONOMIC ASSESSMENT Thickness reduction

The results of calculation, using the pavement design software **BISAR** show that the addition of **natural bitumen** SELENIZZA, increases the stiffness modulus allowing thus a **thickness reduction** of the layer from **8 cm to 6.5 cm**

Layer type	Stiffness Modulus E (MPa)	Poisson's ratio	Layer thickness (cm)
AB 11s	4400	0.35	5
BNS 22s(A)	6585	0.35	8
0/31,5 mm	152	0.40	15
0/63 mm	80	0.40	35

Standard asphalt mixture

Layer type	Stiffness Modulus E (MPa)	Poisson's ratio	Layer thickness (cm)
AB 11s	4400	0.35	5
BNS 22s(A)	8472	0.35	6.5
0/31,5 mm	152	0.40	15
0/63 mm	80	0.40	35

Asphalt mixture with Selenizza



ECONOMIC ASSESSMENTPrices of materials

Component	Content (%)	Mass (kg)	Price of components (€/t)	Price per ton of asphalt mixture (€)
filler	3.4	34.0	4.95	
0/4 mm	38.1	381.0	4.95	
4/8 mm	14.5	145.0	4.95	
8/11 mm	13.5	135.0	4.50	24.60
11/16 mm	7.7	77.0	4.50	
16/22 mm	19.3	193.0	4.50	
Bitumen 50/70	3.5	35.0	573.20	

Standard asphalt mixture

Component	Content (%)	Mass (kg)	Price of components (€/t)	Price per ton of asphalt mixture (€)
filler	3.4	34.0	4.95	
0/4 mm	38.1	381.0	4.95	
4/8 mm	14.5	145.0	4.95	
8/11 mm	13.5	135.0	4.50	25.20
11/16 mm	7.7	77.0	4.50	
16/22 mm	19.3	193.0	4.50	
Bitume 50/70	3.3	35.0	573.20	
50/70 + Selenizza (10 %)	0.3	3.0	560.00	

Asphalt mixture with Selenizza



ECONOMIC ASSESSMENT

	Standard asphalt mixture	asphalt mixture with SLN
Price of materials (€/t)	24.6	25.2
Production cost (€/t)	24.2	26.6
Total (€/t)	48.8	51.8
€/ 1m² x 1cm	1.16	1.25

It can be seen that the addition of SELENIZZA increases the cost of the asphalt mix BNS-22s (A) by **about 7%**

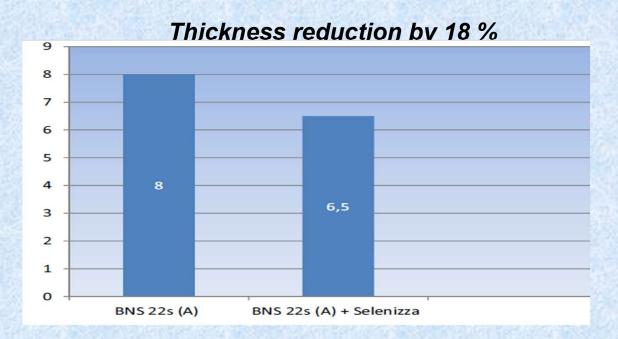
Total unit cost of production of asphalt mixtures with and without the addition of natural asphalt "SELENIZZA"





ECONOMIC ASSESSMENT

On the other hand, there is a possible **thickness reduction** by about **18%**, by using a layer thickness of **6.5 cm** instead of **8 cm**



SELENIZZA

ECONOMIC ASSESSMENT

- Consequently, **the ultimate value** of cost of production of a BNS-22s (A) layer, will be reduced by approximately **13%**
- As an example, for the construction of 1 km BNS-22s (A) layer, on a highway12 meter-wide, by using a layer width of 6,5 cm instead of 8 cm, the needed quantity of the asphalt mixture will be reduced by 430 ton /km, with an ultimate cost saving of 21 000 €/Km compared to the original project



Environmental friendly

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Natural asphalt & environmental assessment

- ➤ Worldwide economical crisis and environmental awareness have created the need for bituminous binders that meet Life Cycle Assessment constraints.
- As a part of a common commitment to sustainable development, the University of Rome in cooperation with the company Selenice Bitumi, carried out e research project, whose aim was to analyze and compare for the first time, the production process of the Albanian natural asphalt (Selenizza) and on the other hand, the various steps necessary to produce the conventional bitumen from crude oil, evaluating the energy consumption and CO₂ emission for each kind of product.



Natural asphalt & environmental assessment

The results of the study showed that:

- The **environmental impact** of the production processes for the bitumen Selenizza (in terms of **CO₂ production**) is about **half** the impact of the road bitumen produced in oil refineries.
- Energy consumption is **reduced** as well, to about **half** the value of the bitumen produced from crude oil.



Production & reference sites

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Podgorica 2015 – Natural Asphalt Selenizza



exploitation in an open-pit quarry









exploitation in an open-pit quarry





exploitation in an open-pit quarry





Crude ore before melting





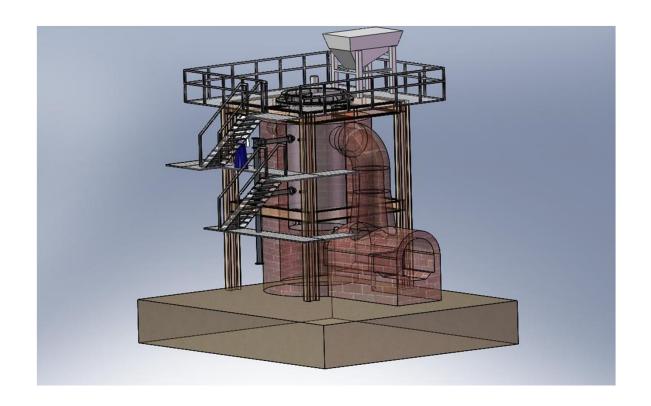
The blocks of asphalt are selected before the melting





transport into the furnace via conveyor belt





Furnace for bitumen melting at the temperature of about 200 - 240°C





Production capacity of 7,000 tons per year





After melting, the cleaned bitumen is poured into hexagonal moulds



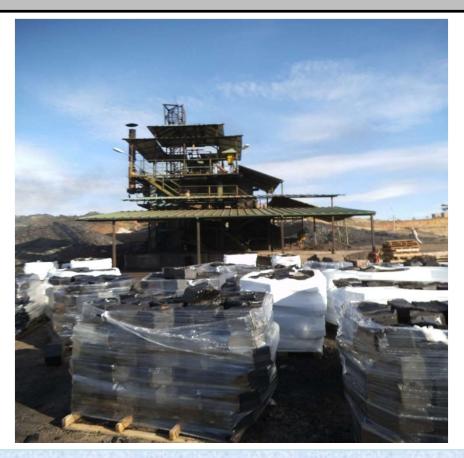


Each production batch is identified by a lot number





Analysis are carried out, checking and recording the parameters for every batch



Every single production batch is located in a parcel clearly identifiable









The clean bitumen hexagonal blocks are grinded in powder 0/6mm or in granular form 6/12 mm



The Packaging: big bags of about 1 ton and polyethylene, thermofusible bags of 15kg

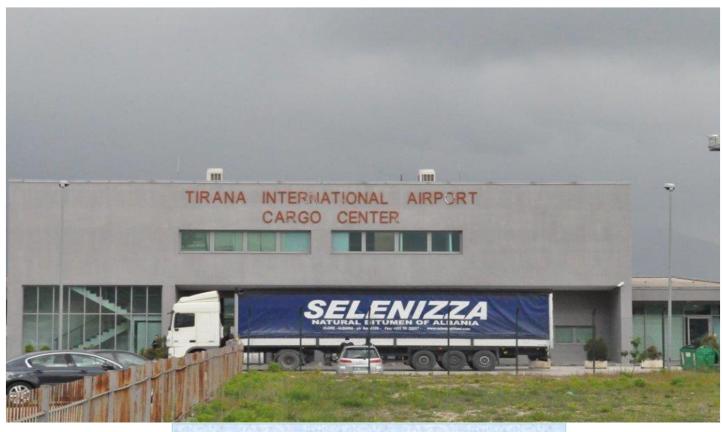
SELENIZZA











Transport by truck





Maritime transport :Vlora port (Al)





Maritime transport : cargo loading





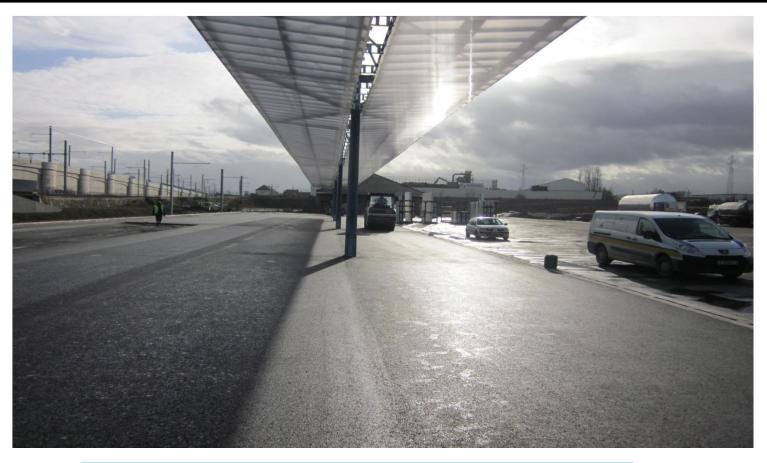
Bitumen transport aboard cargo plane





Bus lane Chartres France





Tramway Dijon(France)





2011: Bridge in Val de Verzaska, Ticino - Switzerland





Mastic asphalt Switzerland





Mastic asphalt sidewalk Berne - Switzerland





Mastic asphalt Berne - Switzerland









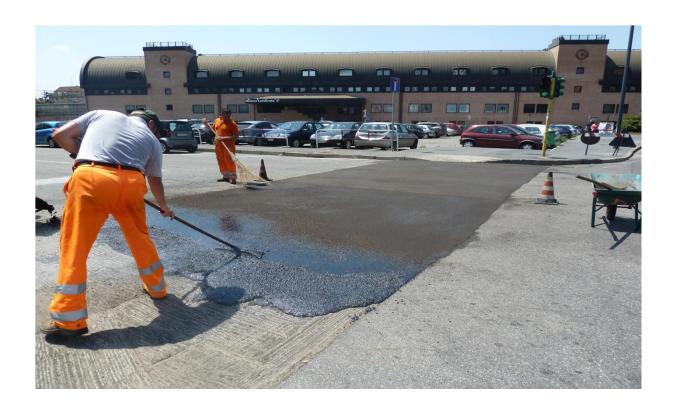




















Highway Ticino- Switzerland





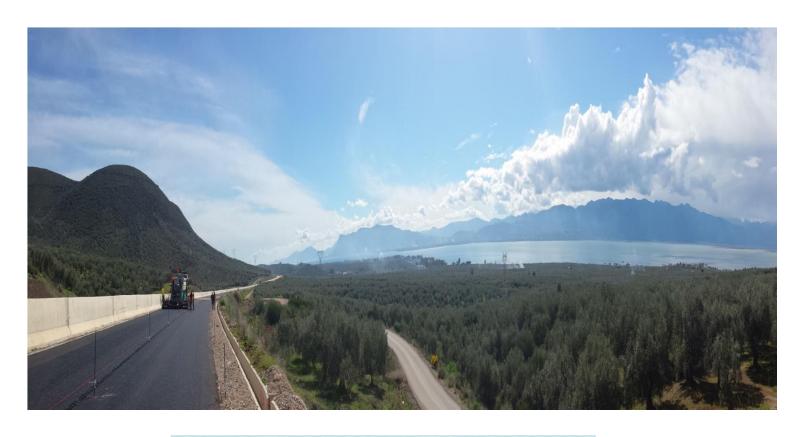
2014: Motorway A 150 - France





2014: Port Le Havre - France





2014: Motorway Stylida - Grèce





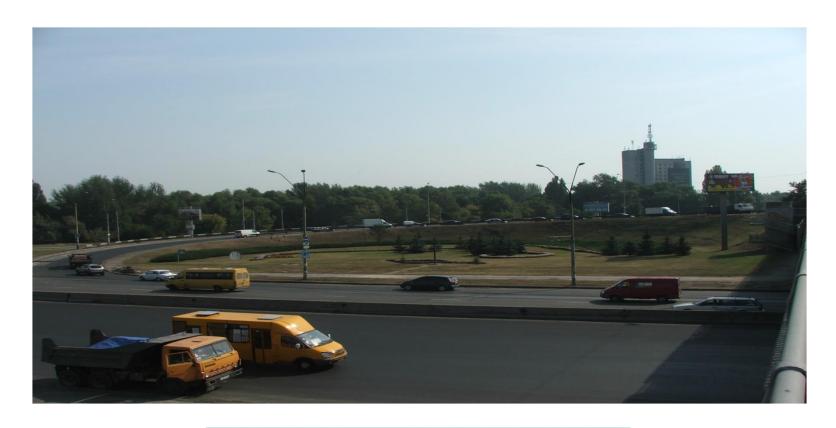
2013 : Motorway Thessalonique - Grèce





2011: Bern motorway ring -Switzerland





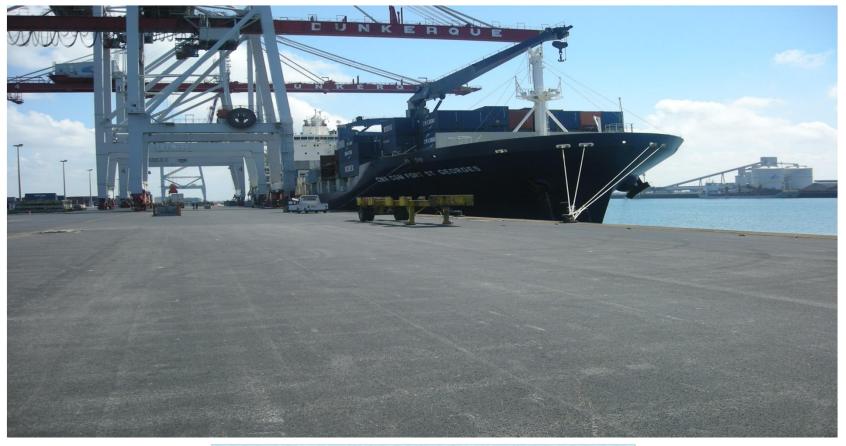
Ring road Kiev (Ukraina)





National Road Mykolaiv (Ukraina))





Port Le Havre 2 000 (France)





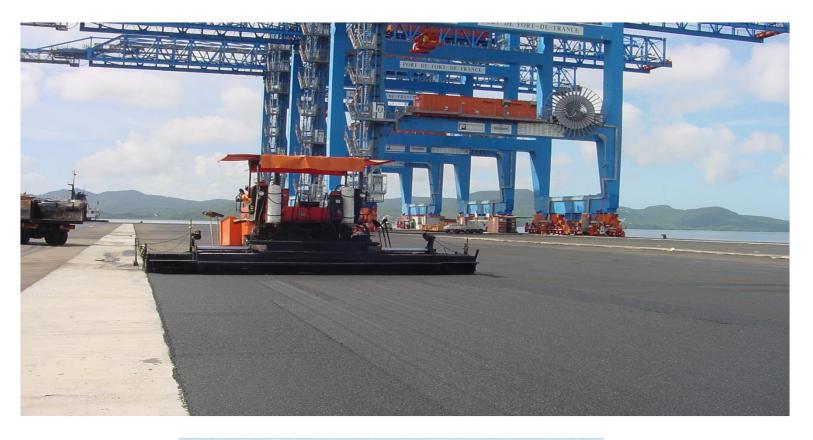
Road junction (France)





Port Martinique (France)





Port French Antilles





Port platform (France)





Airport Fort de France





Port Martinique (France)



Conclusion

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Conclusion

- ➤ 100% compatible with bitumen from refinery (and polymer modified bitumens)
- High performance in modulus & permanent deformation
- Better bitumen-aggregates adhesion
- Pavement thickness reduction
- Better workability
- Higher lifetime of the pavements





Thank you for your attention!